

Advanced Control of Microgrids

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Presented at

The Great Lakes Symposium on Smart Grid and the New Energy Economy

Chicago, September 2012

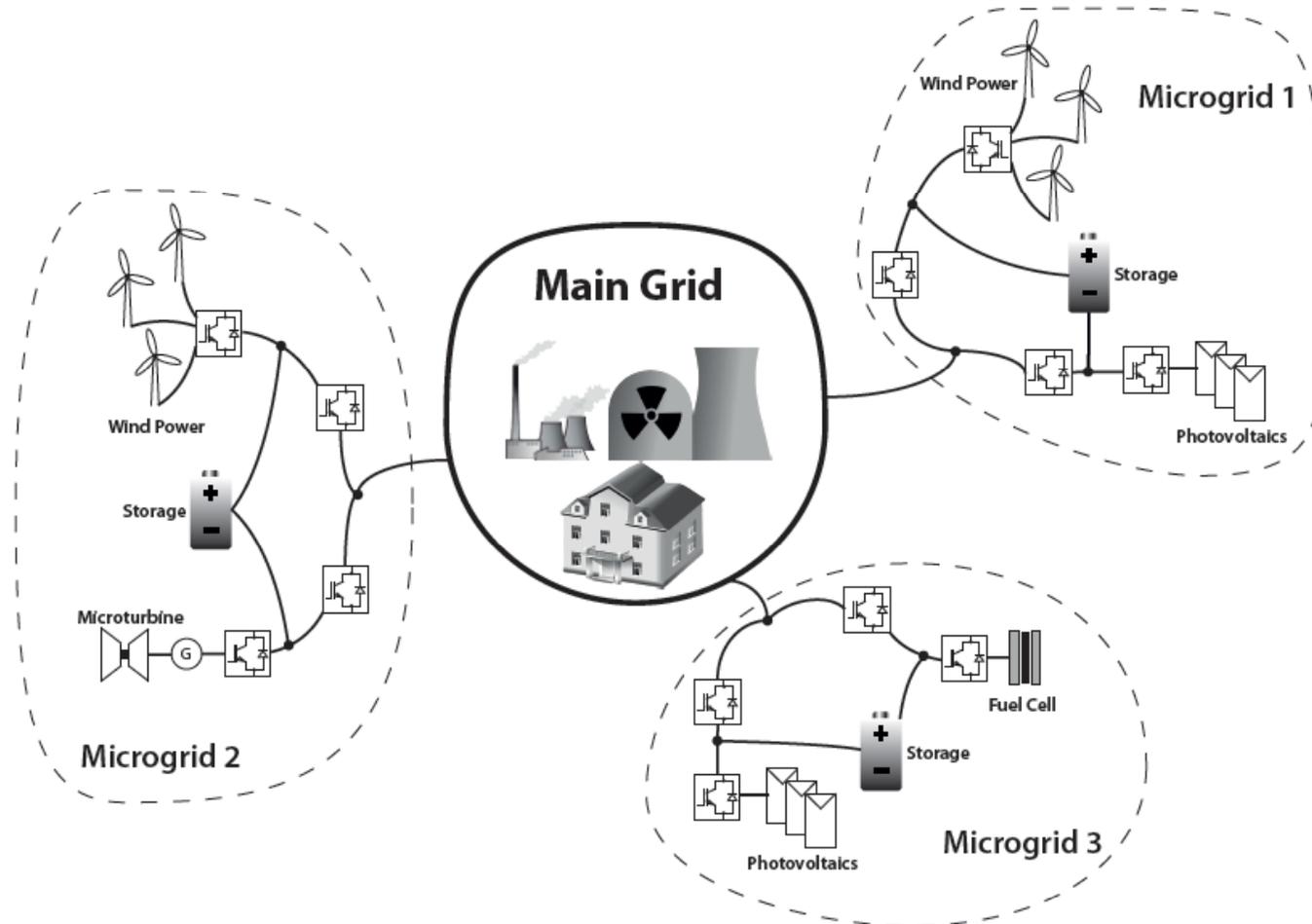
This presentation is a summary of the following paper:

- B.Bahrani , M. Saeedifard, A. Karimi, A.Rufer, “A Multivariable Design Methodology for Voltage Control of a Single-DG-Unit Microgrid,” accepted for publication in the IEEE Trans. on Industrial Electronics.

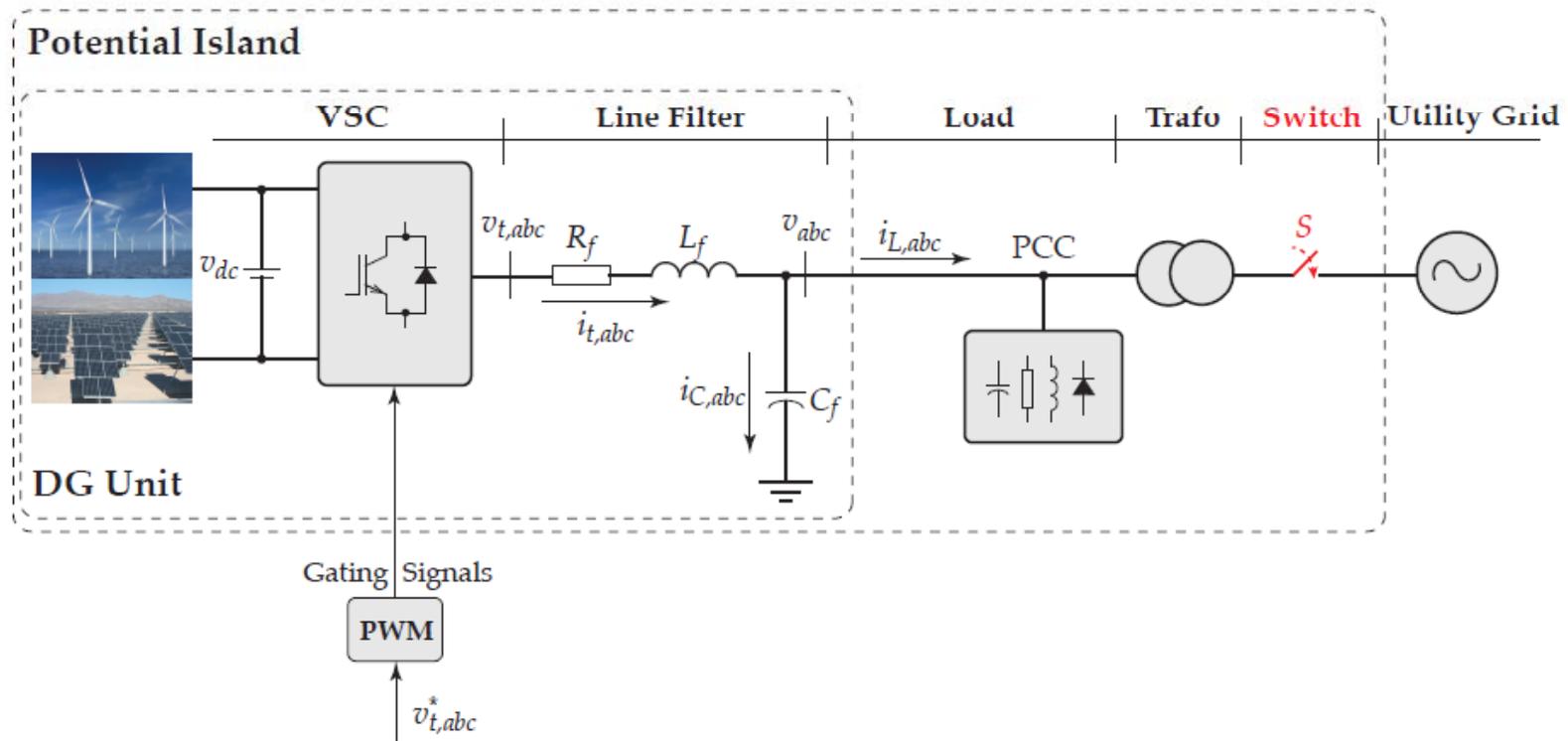
Outline

- Introduction
- Statement of the Problem
- The Proposed Multivariable Controller
- Experimental Results
- Conclusions

Introduction

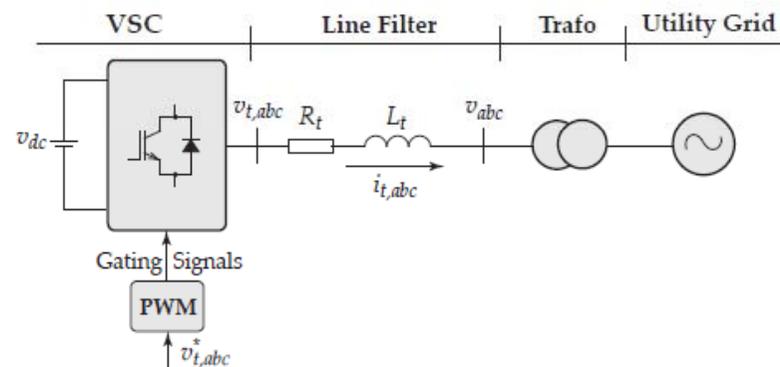
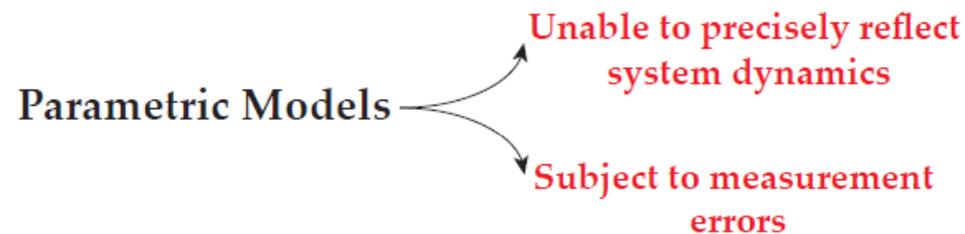


Introduction



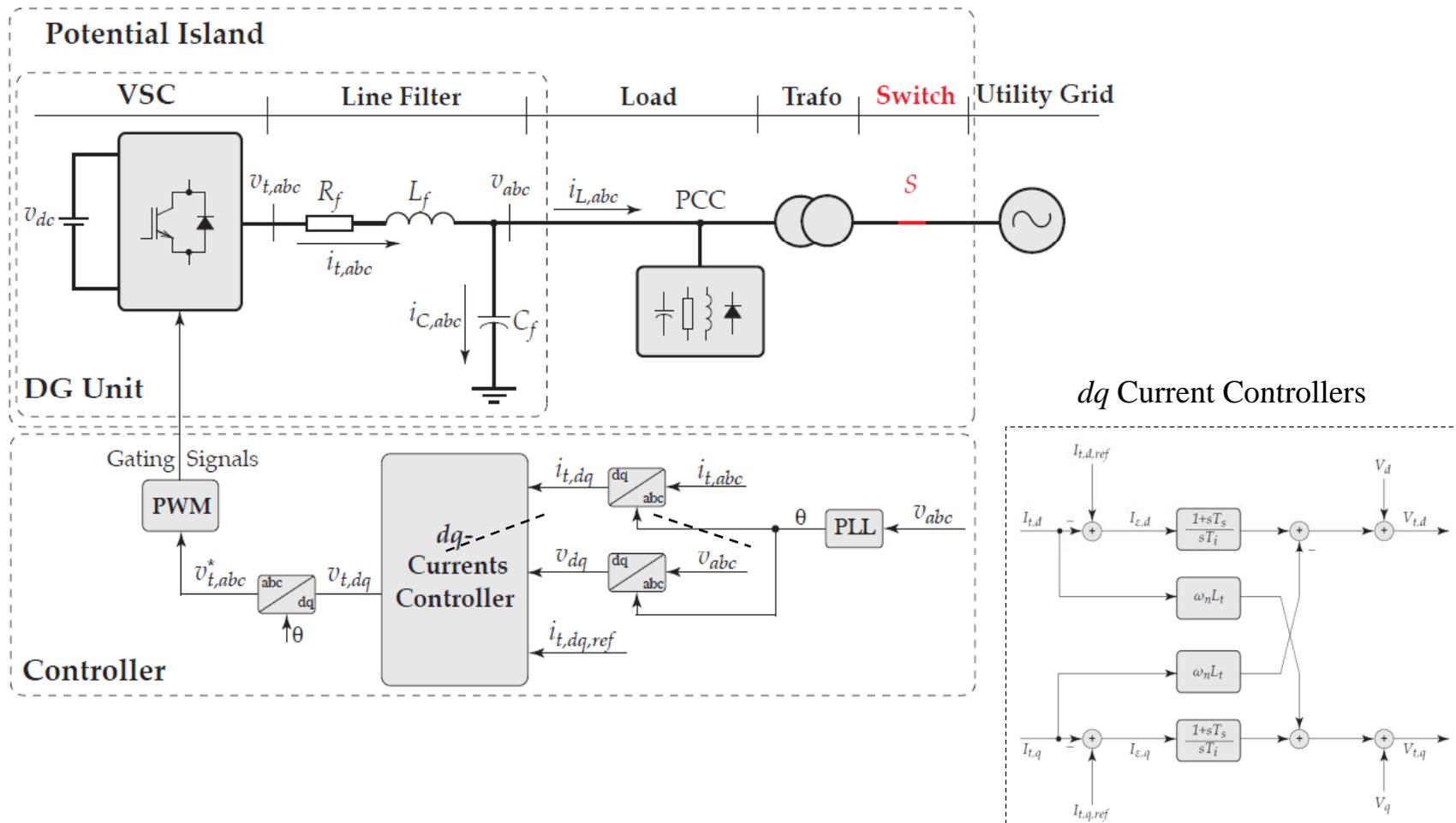
Introduction

- To design controllers, the model of the to-be-controlled system is essential.



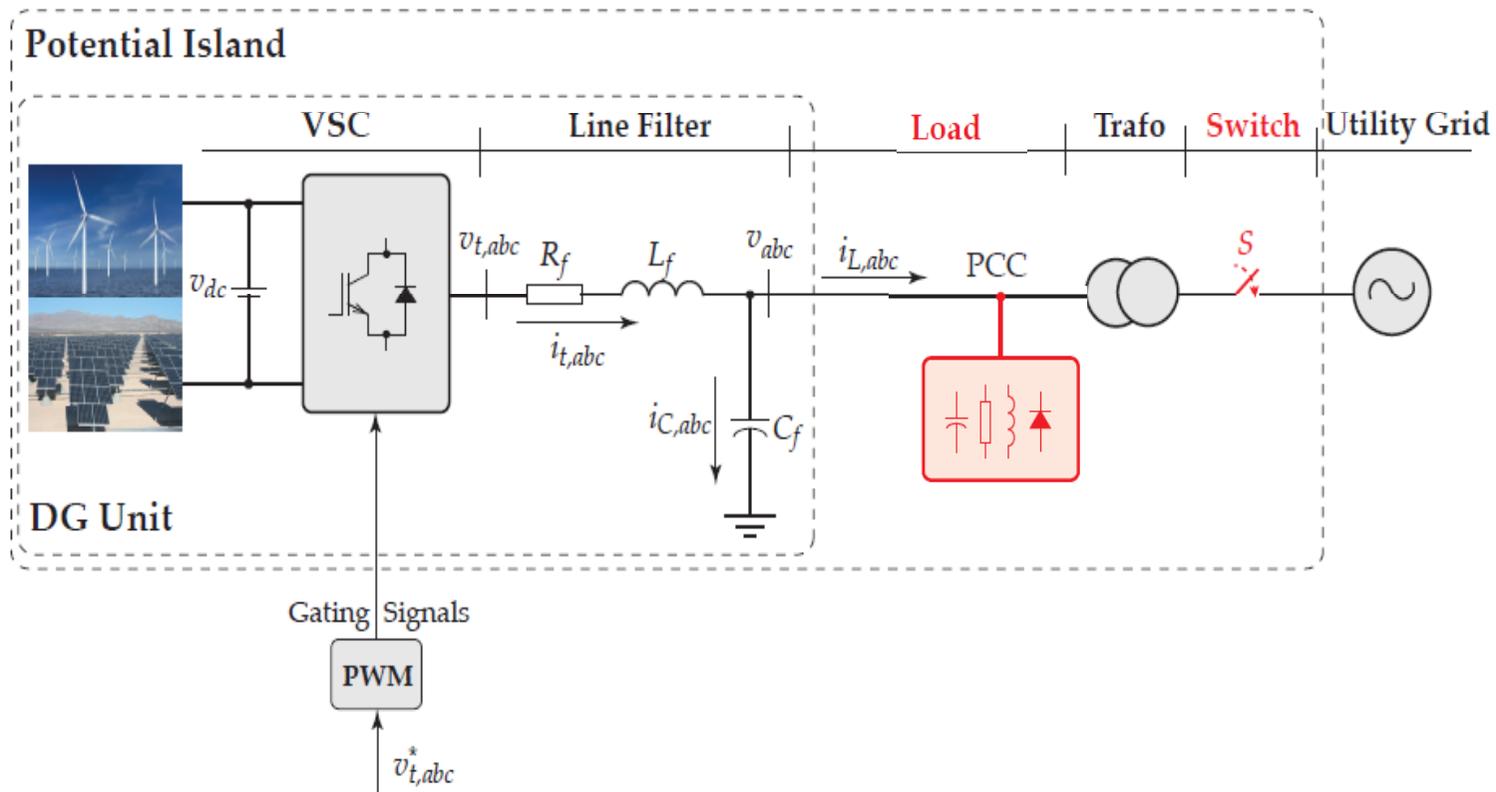
Introduction

- Current Control of a Grid-connected Microgrid



Statement of the Problem

- Robustness issues to uncertainties in the load parameters
- Distortion of the load voltage in presence of harmonically polluted loads

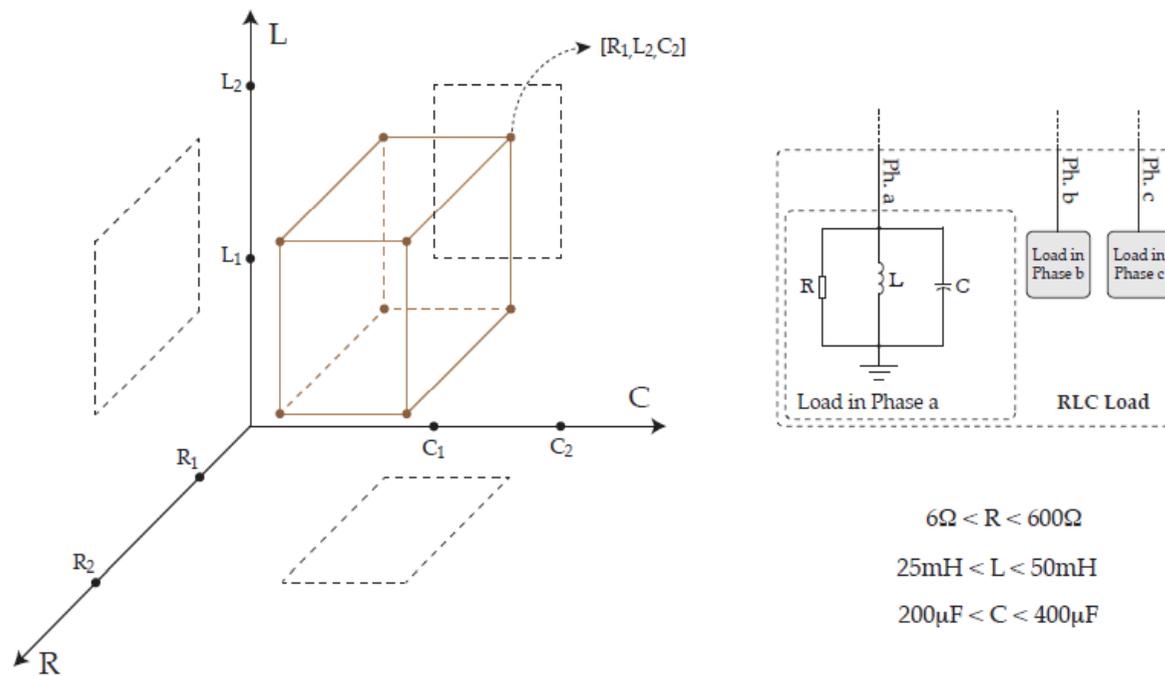


The Proposed Multivariable Controller

- The proposed design approach, initially proposed in [1], relies on shaping the open-loop and closed-loop transfer functions of the system through convex optimization.
- The design procedure consists of three steps:
 - Step 1.** Determination of the (family of) spectral or nonparametric model(s) of the system
 - Step 2.** Determination of the controller class
 - Step 3.** Determination of the controller coefficients

The Proposed Multivariable Controller

Step 1. Determination of the (family of) spectral or nonparametric model(s) of the system



The Proposed Multivariable Controller

Step 1. Determination of the (family of) spectral or nonparametric model(s) of the system

$$\begin{bmatrix} V_d \\ V_q \end{bmatrix} = \underbrace{\begin{bmatrix} G_{i,11} & G_{i,12} \\ G_{i,21} & G_{i,22} \end{bmatrix}}_{\mathbf{G}_i} \begin{bmatrix} V_{t,d} \\ V_{t,q} \end{bmatrix}$$

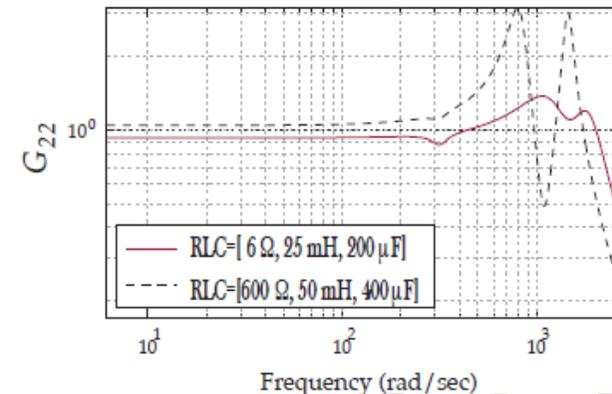
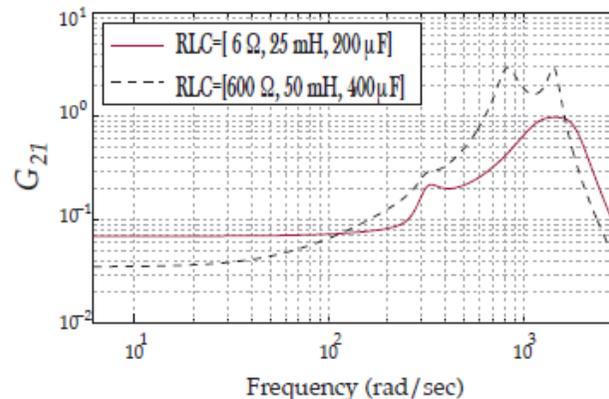
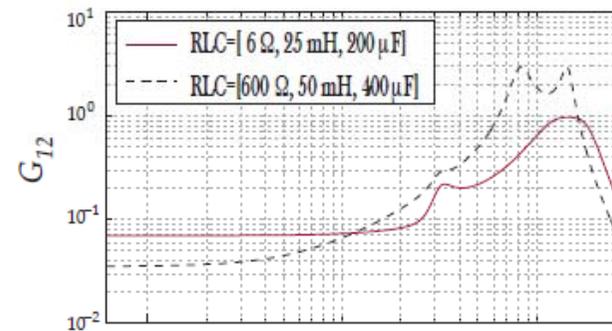
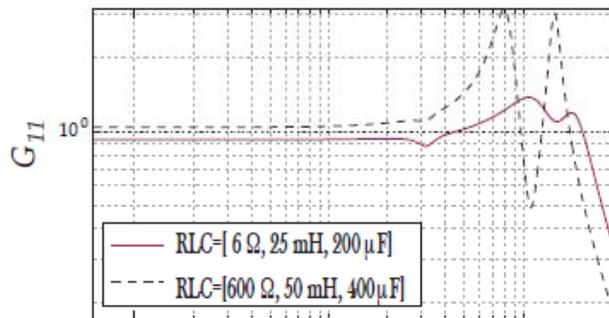
$$G_{i,11}(j\omega) = \frac{\mathcal{F}(v_d)}{\mathcal{F}(v_{t,d})} \quad \text{and} \quad G_{i,21}(j\omega) = \frac{\mathcal{F}(v_q)}{\mathcal{F}(v_{t,d})}$$

$$G_{i,12}(j\omega) = \frac{\mathcal{F}(v_d)}{\mathcal{F}(v_{t,q})} \quad \text{and} \quad G_{i,22}(j\omega) = \frac{\mathcal{F}(v_q)}{\mathcal{F}(v_{t,q})}$$

$$\mathcal{G} = \{\mathbf{G}_i(j\omega); i = 1, \dots, 8; \forall \omega \in \mathbb{R}\}$$

The Proposed Multivariable Controller

Step 1. Determination of the (family of) spectral or nonparametric model(s) of the system



The Proposed Multivariable Controller

Step 2. Determination of the class of the controller

$$\mathbf{K}(z, \rho) = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix}, \text{ and therefore, } \mathbf{L}(j\omega, \rho) = \mathbf{G}(j\omega) \mathbf{K}(j\omega, \rho)$$

- **Multivariable-Proportional Integral (PI)-Resonant Controller**

$$K_{21}(z) = \frac{\rho_4 + \rho_5 z^{-1}}{1 - z^{-1}} + \rho_6 \frac{b_1 z^{-1} + b_2 z^{-2}}{1 + a_1 z^{-1} + a_2 z^{-2}}$$

The Proposed Multivariable Controller

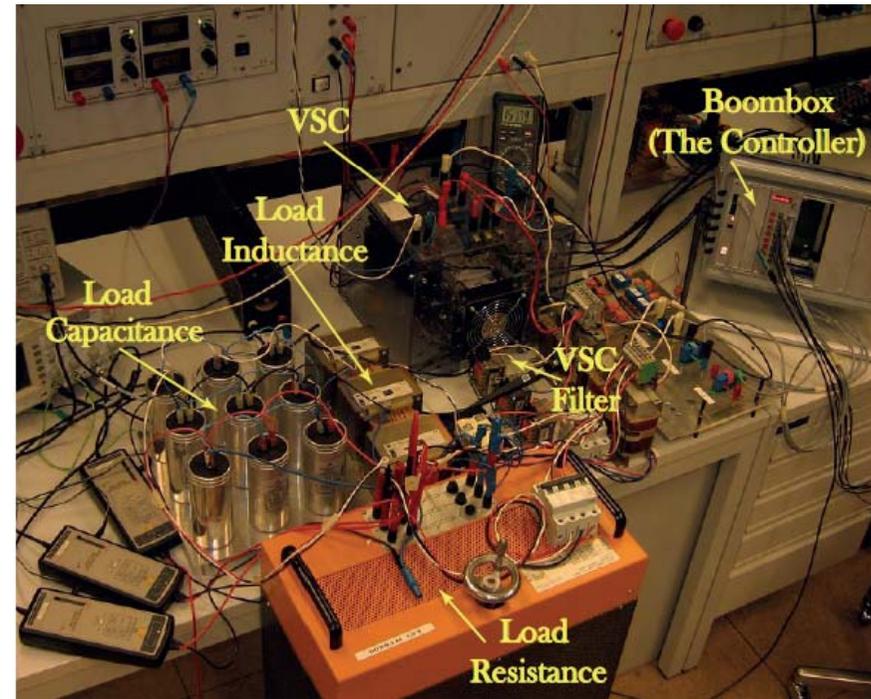
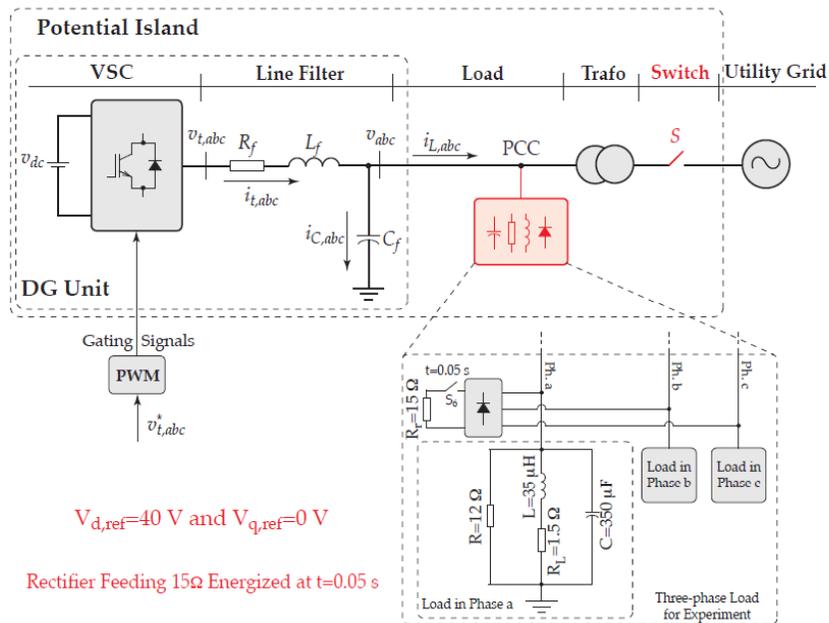
Step 3. Determination of the controller coefficients by loop-shaping

The open-loop shaping the system with a family of \mathcal{G} is carried out by the following minimization

$$\min_{\rho} \sum_{i=1}^m \| \mathbf{L}_i(\rho, j\omega) - \mathbf{L}_D(j\omega) \|^2, \quad \mathbf{L}_D(s) = \begin{bmatrix} \frac{\omega_{c1}}{s} + \frac{\omega_{c2}}{s^2 + 2\zeta\omega_h s + \omega_h^2} & 0 \\ 0 & \frac{\omega_{c1}}{s} + \frac{\omega_{c2}}{s^2 + 2\zeta\omega_h s + \omega_h^2} \end{bmatrix}$$

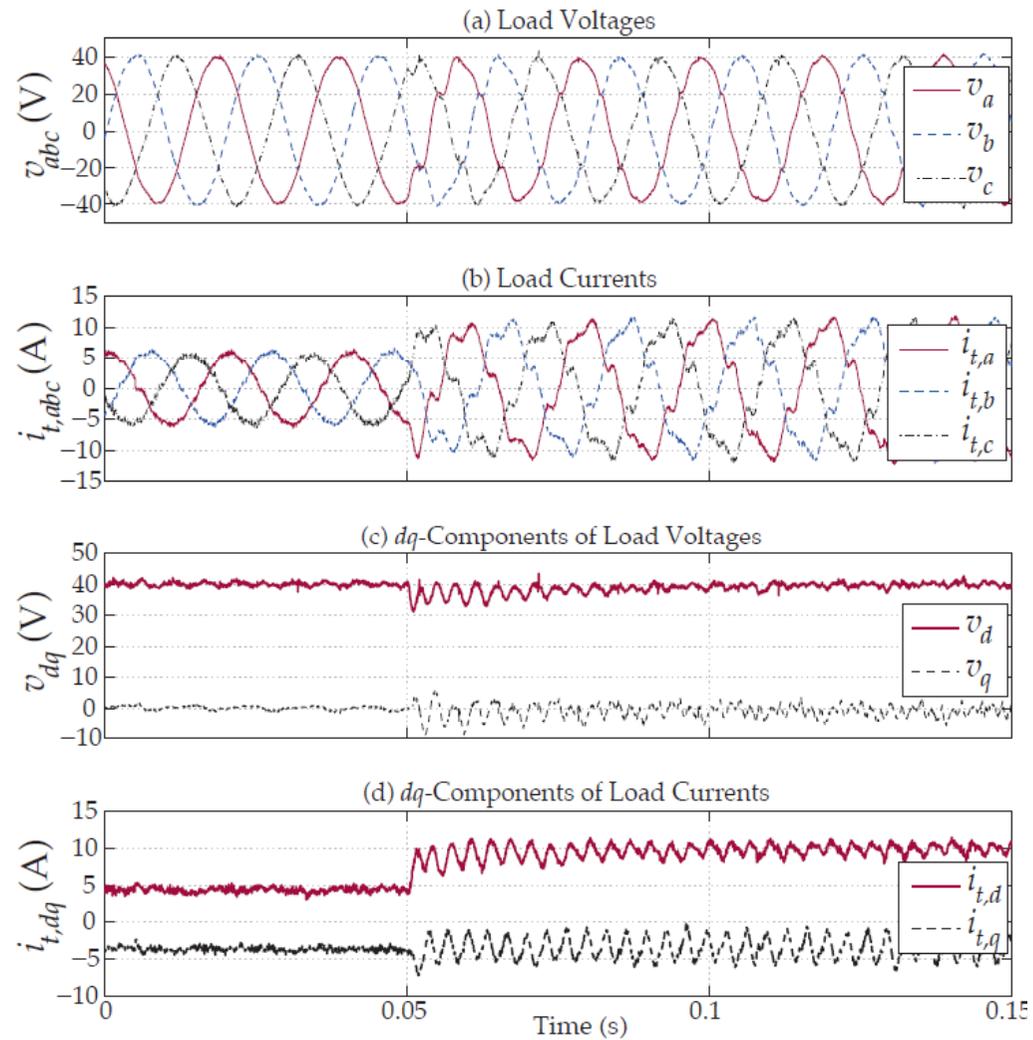
Experimental Setup

Nonlinear Resistive Load Change



Experimental Results

Nonlinear at $t=0.05$ s



Conclusions

- A voltage controller for islanded microgrids have been proposed.
- The proposed controller provides satisfactory dynamic performance and robustness in the presence of nonlinear loads.